

Contributions of Material and Geometric Properties to Structural Response in Anterior-Posterior Loading of Human Ribs

Akshara Sreedhar¹, Yun-Seok Kang¹, Devon Albert², Andrew Kemper², Amanda Agnew¹

¹Injury Biomechanics Research Center, The Ohio State University, ²Center for Injury Biomechanics, Virginia Tech

INTRODUCTION

- Thorax injuries, specifically rib fractures, are common in motor vehicle crashes and can lead to high rates of morbidity and mortality (Kent et al. 2008). Creating biofidelic finite element models is important for improving thoracic injury countermeasures, but can only be achieved using accurate properties of human ribs in dynamic loading (Murach et al. 2017).
- Previous studies have identified relationships between structural response of ribs and material and geometric properties individually. However, these relationships only explained a small amount of variance in structural properties. Additionally, the combined contributions of these properties has yet to be investigated in regard to explaining variability in whole rib structural response.
- The goal of this study was to quantify the contributions of human rib material and geometric properties to the variation in whole rib structural response.

MATERIALS & METHODS

• Thirty-seven 6th level rib pairs from fresh post-mortem human subjects (16 female, 21 male, 24-99 years) were selected for direct comparison of properties.

Structural Dynamic Bending Testing

 One randomly selected left or right whole rib was tested in a 2D dynamic bending scenario, simulating a frontal impact to the thorax by translating the sternal end toward the fixed vertebral end (Figure 1). Structural properties were calculated from force vs. displacement curves (Figure 2).

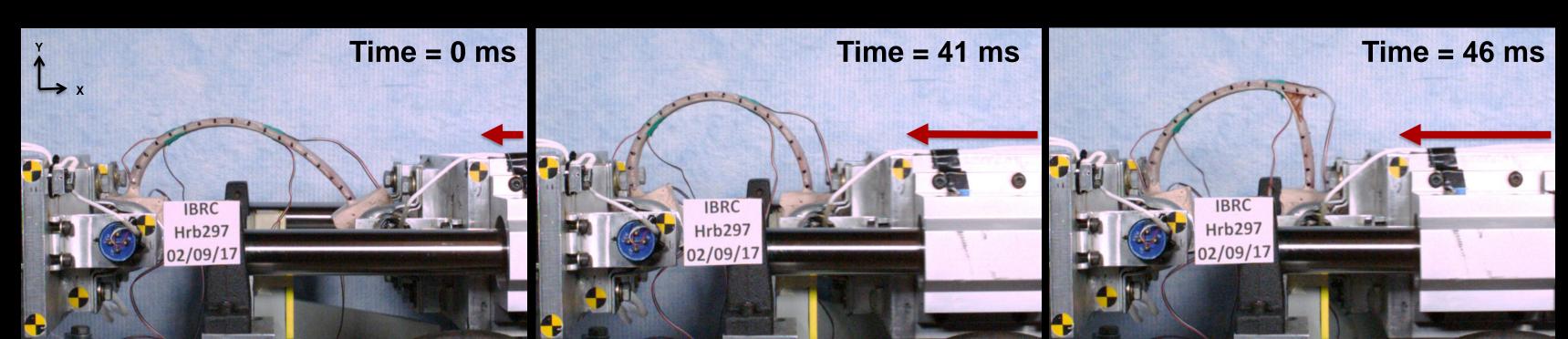


Figure 1: Dynamic bending test on whole human rib for structural properties

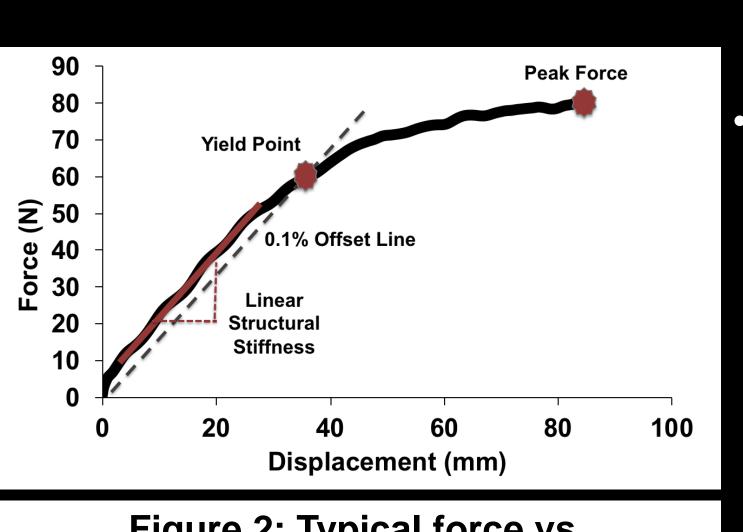
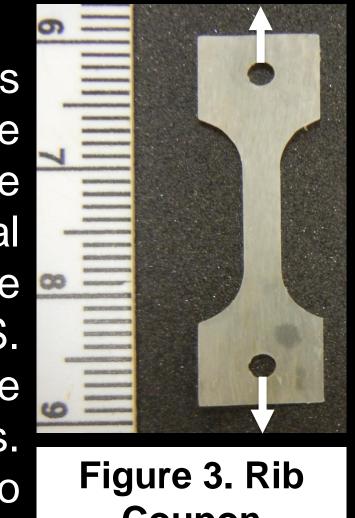


Figure 2: Typical force vs. displacement curve

Material Testing

contralateral rib was used to obtain cortical bone coupons (Figure 3) from the cutaneous cortex for uniaxial tensile tests on a high-rate 810 servo-hydraulic MTS. Material properties calculated from the stress vs. strain curves analogous to structural properties.



Coupon

For maximum comparability, all yield-dependent calculations were made using a 0.1% offset method in structural and material properties. All structural and material tests were conducted at ~0.5 strain/sec for direct comparison.

Geometric Properties

After dynamic bending tests, high resolution (1446 pix/mm) microscopic obtained images were from a section adjacent to location fracture the (Figure 4). Cross-sectional geometric properties such as Whole Bone Strength Index (WBSI), Robusticity, and Cutaneous Cortical Thickness (Cut.Ct.Th) calculated using were MATLAB and ImageJ.

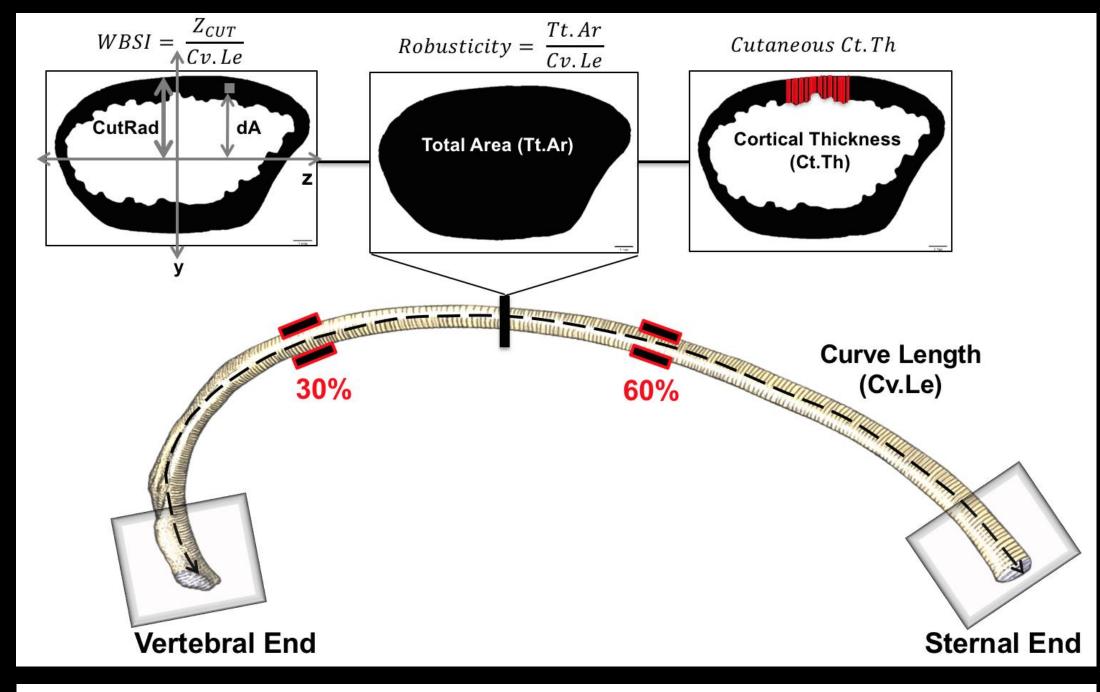


Figure 4: Cross-sectional property calculations

REFERENCES CITED - Kent, R., Woods, W., & Bostrom, O. (2008). Fatality Risk and the Presence of Rib Fractures. Annals of Advances in Automotive Medicine, 52(October), 73–82. - Murach, M.M., Kang, Y.-S., Goldman, S.D., Schafman, M.A., Schlecht S.H., Moorhouse K., Bolte IV, J. H., Agnew A.M. (2017). Rib Geometry Explains Variation in Dynamic Structural Response: Potential Implications for Frontal Impact Fracture Risk. Annals of Biomedical Engineering, 45(September), 2159-2173.

RESULTS & DISCUSSION

Table 1: Multiple Regression Results						
Structural Property	Material Property		Geometric Property		Model	
Stiffness	Modulus 1.20%	p-value 0.351	WBSI 53.18%	p-value <0.0001	R ² 54.38%	p-value < 0.0001
	Modulus	p-value	Robusticity	p-value	R^2	p-value
	2.98%	0.119	57.25%	<0.0001	60.23%	<0.0001
	Modulus	p-value	Ct.Th	p-value	R^2	p-value
	0.17%	0.794	15.63%	0.021	15.80%	0.054
Displacement in X at Yield	Yield Strain	p-value	WBSI	p-value	R^2	p-value
	0.38%	0.713	6.42%	0.127	6.80%	0.302
	Yield Strain	p-value	Robusticity	p-value	R^2	p-value
	0.01%	0.953	21.82%	0.004	21.83%	0.015
	Yield Strain	p-value	Ct.Th	p-value	\mathbb{R}^2	p-value
	0.05%	0.898	6.31%	0.141	6.35%	0.328
Force in X at Yield	Yield Stress	p-value	WBSI	p-value	R ²	p-value
	8.08%	0.04	31.65%	<0.0001	39.73%	<0.0001
	Yield Stress 12.47%	p-value 0.02	Robusticity 15.85%	p-value 0.006	28.32%	p-value 0.003
	Yield Stress	p-value	Ct.Th	p-value	R ²	p-value
	2.54%	0.193	48.58%	<0.0001	51.12%	
Peak Strain	Ultimate Strain	p-value	WBSI	p-value	R^2	p-value
	19.70%	0.012	0.59%	0.881	20.29%	0.037
	Ultimate Strain	p-value	Robusticity	p-value	R^2	p-value
	21.86%	0.008	0.39%	0.392	22.25%	0.026
	Ultimate Strain	p-value	Ct.Th	p-value	R^2	p-value
	6.16%	0.113	26.78%	0.026	32.94%	0.003
Peak Force	Ultimate Stress	p-value	WBSI	p-value	R^2	p-value
	0.98%	0.434	47.78%	<0.0001	48.76%	<0.0001
	Ultimate Stress	p-value	Robusticity	p-value	R^2	p-value
	0.10%	0.813	41.12%	<0.0001	41.22%	<0.0001
	Ultimate Stress	p-value	Ct.Th	p-value	R^2	p-value
	1.66%	0.366	33.24%	<0.0001	34.90%	<0.0001
Total Energy	Strain Energy Density	p-value	WBSI	p-value	R ²	p-value
	27.19%	0.001	5.19%	0.287	32.38%	0.002
	Strain Energy Density	p-value	Robusticity	p-value	R^2	p-value
	27.81%	0.001	5.73%	0.193	33.54%	0.001
	Strain Energy Density	p-value	Ct.Th	p-value	R^2	p-value
	18.50%	0.006	11.80%	0.697	30.30%	0.003
Elastic Energy	Elastic Strain Energy Density	p-value	WBSI	p-value	R^2	p-value
	4.00%	0.216	12.87%	0.047	16.87%	0.047
	Elastic Strain Energy Density	p-value	Robusticity	p-value	\mathbb{R}^2	p-value
	2.41%	0.325	17.82%	0.015	20.23%	0.024
	Elastic Strain Energy Density	p-value	Ct.Th	p-value	R ²	p-value
		•		•		
	2.67%	0.331	6.65%	0.191	9.32%	0.199

- Using multiple regression models, results show the contribution of each predictor, an analogous material property and various geometric properties, in regard to explaining variation in each structural property (Table 1). Geometric properties had a larger role in determining structural response variables except for the total energy analyses. This was intuitive because energy absorption and resistance to deformation, prior to fracturing, are highly dependent on material composition.
- Structural properties have been found to be highly correlated with overall bone size and shape (Murach et al. 2017). This was evident in the stiffness relationships, where robusticity explained 57% of variance while modulus only explained 3%.
- The amount of variance explained by the models was relatively low $(R^2=9-60\%)$ suggesting additional predictors should be explored. Furthermore, utilizing alternate modeling techniques may improve our characterization of variability in whole rib response.

CONCLUSIONS

- Multiple regression models are useful tools to better understand sources of variation in rib structural properties. The current models revealed that geometric properties play a larger role in the structural response of human ribs than material properties.
- The results from this study and future work will be crucial to advancing finite element human body models by providing essential material and geometric properties of ribs and how they contribute to overall rib and thoracic response, with the ultimate goal of reducing thoracic injury risk from motor vehicle crashes.

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